

Production and conversion of liquid fuels and hydrogen from biomass and natural gas using micro-reactor technology

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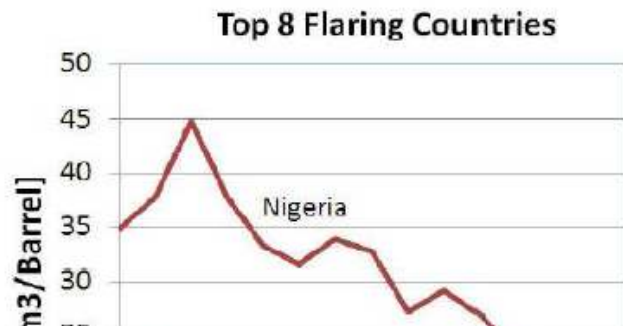
- Motivation
- Methods of catalyst application
- Fuel routes and current projects
- Reactor design for lab-scale testing
- **Applications and results from laboratory**
- Scale-up / feasibility
- Conclusion

Motivation

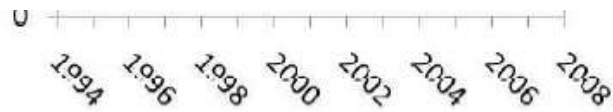
- Flexible and compact systems for fuel production are needed worldwide for application to

off-shore stranded (flared) natural gas

$\sim 0,04 \text{ m}^3(\text{gas})/\text{l}(\text{oil})$



A own tentative LC analysis shows 3% increase in net energy and a possible reduction of CO₂ on-site of about 40% with a micro-GTL system



C. D. Elvidge, *Energies* 2, 595 (2009).



Satellite photo of Nigeria showing gas flaring

Flaring on a oil platform

Motivation

- Flexible and compact systems for fuel production are needed worldwide for application to

Virginia farmland

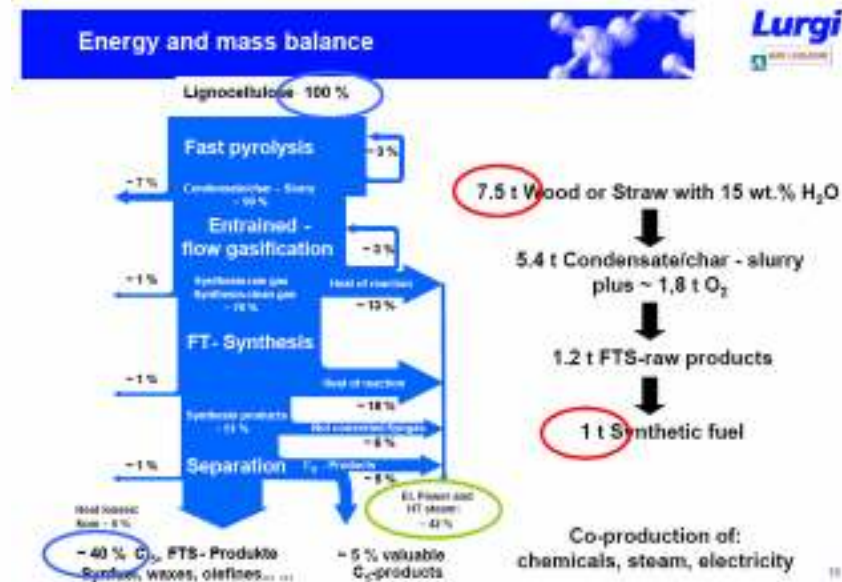


Straw as source



small scale biomass gasifiers

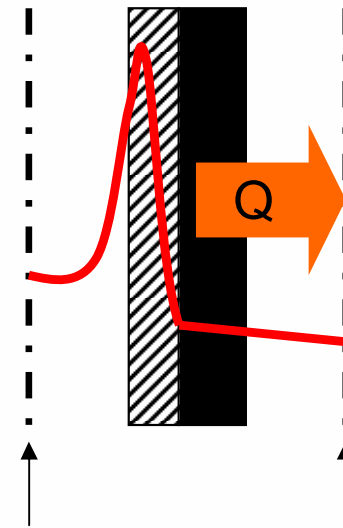
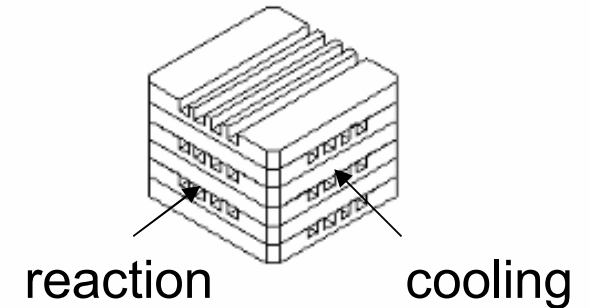
- minimize space (nicely fit into environment)
- cope with different feed (waste, straw etc.)
- competitive with large scale synthesis



<http://www.greencarcongress.com/2008/12/air-liquide-mov.html>

Motivation

- Microreactors allow the control of fast, highly energetic reactions
 - due to good heat transfer
 - in the wall: λ/s is not limiting
 - in the fluid: laminar $\Rightarrow Nu = \text{const.}$
- $$\Rightarrow \alpha \sim d^{-1}$$
- due to absence of mass transfer limitations (diffusion length is small)
- BUT: A low specific loading with catalyst
 - \Rightarrow High reaction rates are necessary to avoid manufacture costs consequences
 - \Rightarrow chance for preventing new and highly active catalysts of deactivation
 - Easy control of performance / conversion at changing feed



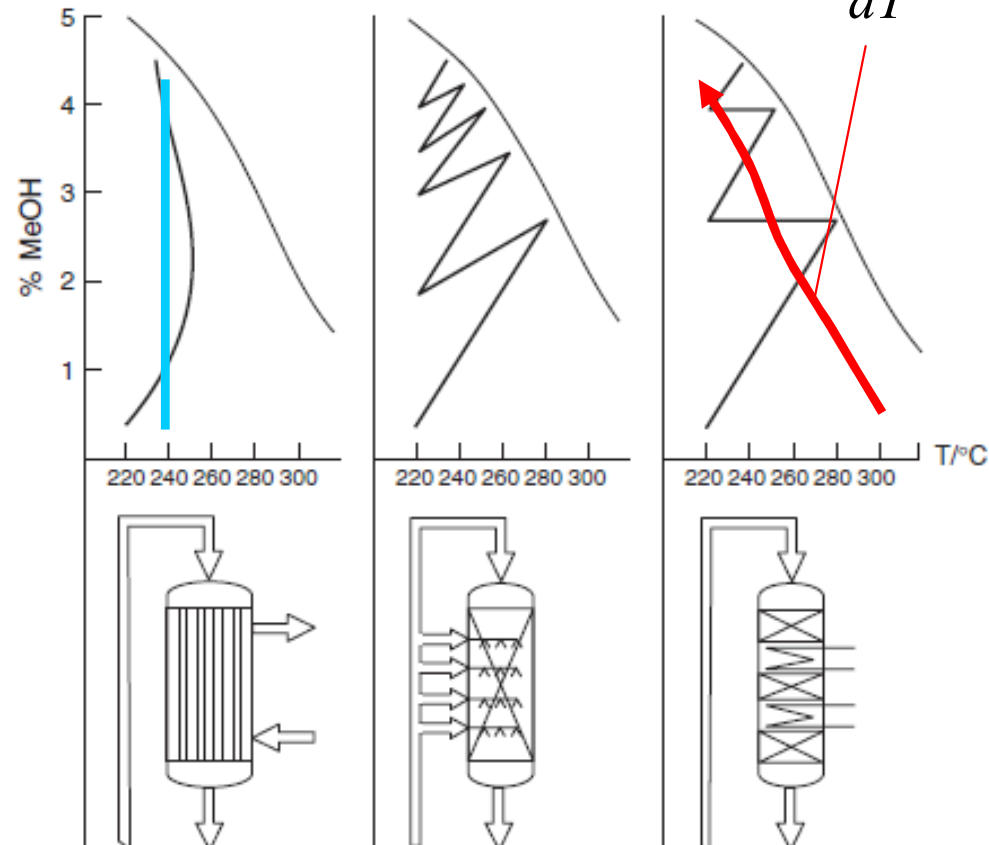
Motivation

- A optimized falling temperature profile can be established for exothermic fuel synthesis

Isothermal

Optimum trajectory: $\frac{dr(X)}{dT} = 0$

$$r = k_o e^{\left(\frac{-E_A}{RT}\right)} \left(x_a x_b - \frac{x_c x_d}{K(T)} \right)$$



Hansen, J.B. and P.E. Højlund Nielsen, Methanol Synthesis, in Handbook of Heterogeneous Catalysis. 2008: Wiley-VCH

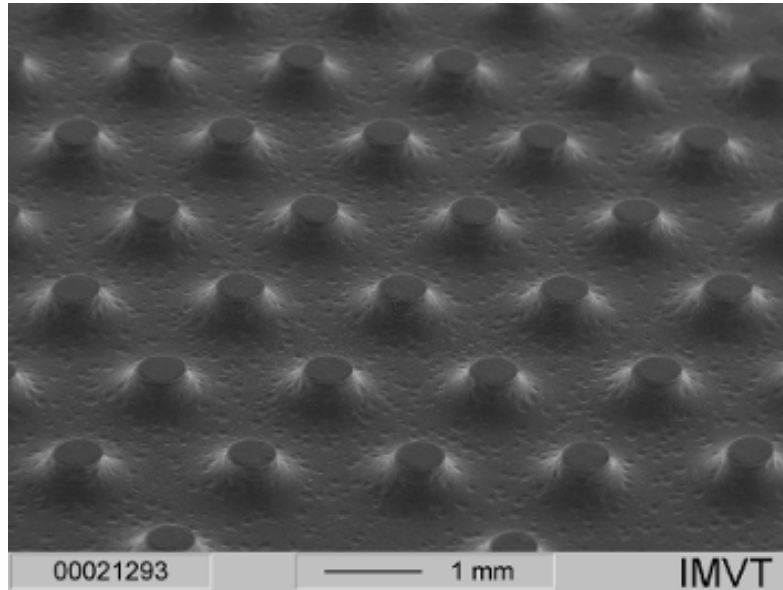
- Less heat loss due to smaller reactors
- Cooling fluid leaves the system with high temperature

⇒ efficient scale-down for “small scale” utilization of resources

Methods of catalyst incorporation

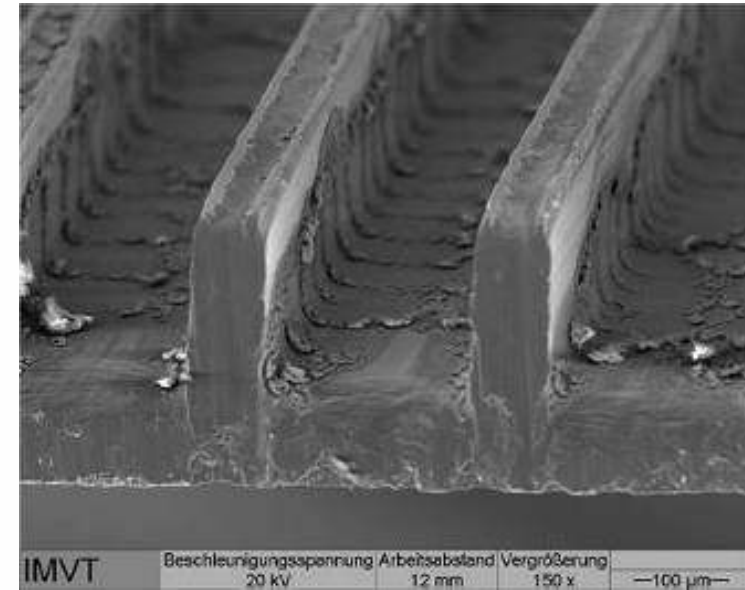
- Two different concepts

Catalyst packing (“micro fixed bed“)



Comparable
STY possible

Coated channel walls

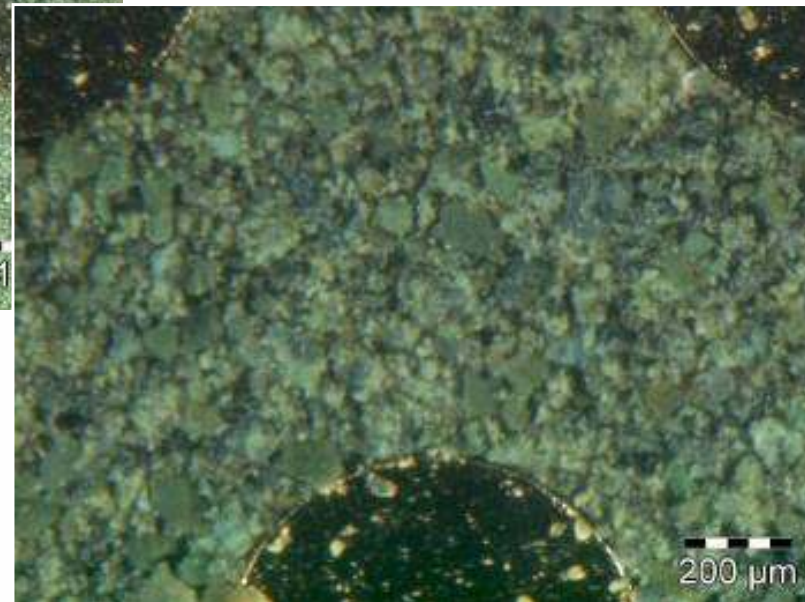
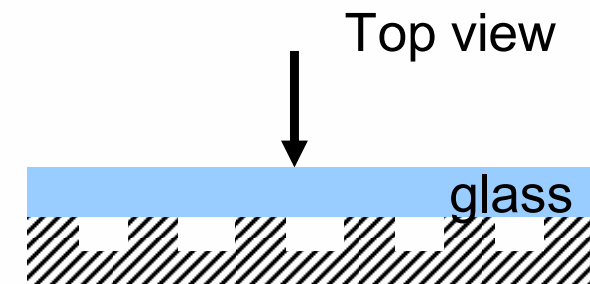
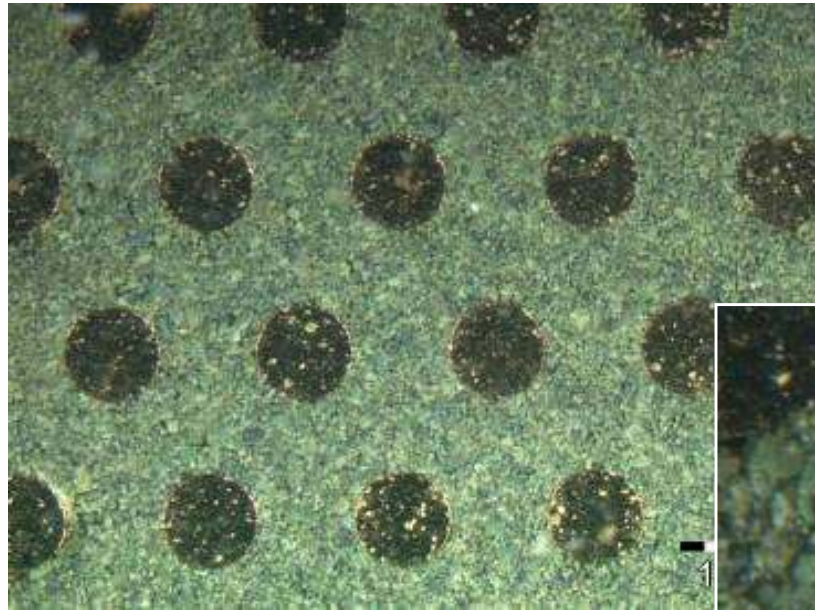


- *High catalyst amount per volume*
(V_{cat}/V_R up to 50 %)
- *Conventional catalysts applicable (powder)*
- *Catalyst easy to be replaced*

- *Excellent temperature control*
- *Suitable for highly active catalysts*
($>20 \text{ kg}_{Prod.}/\text{kg}_{cat} \cdot \text{h}$)
- *Coating process to be developed*
(adhesion, etc.)

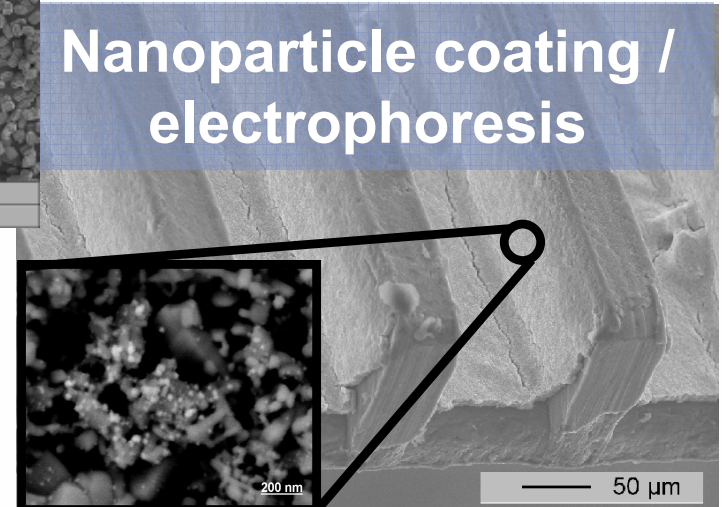
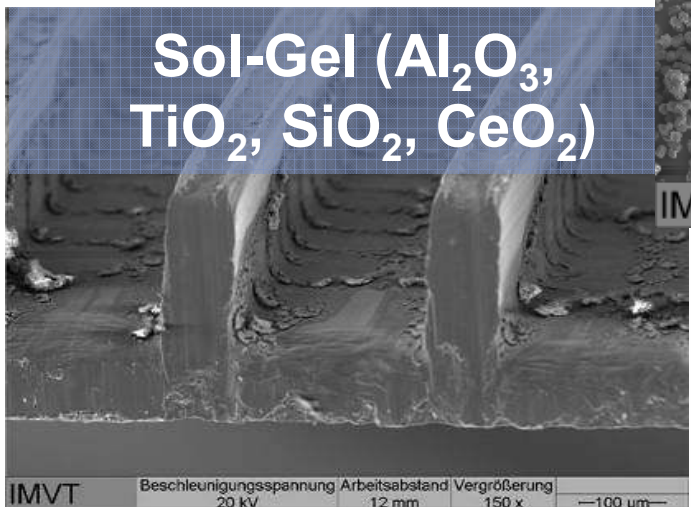
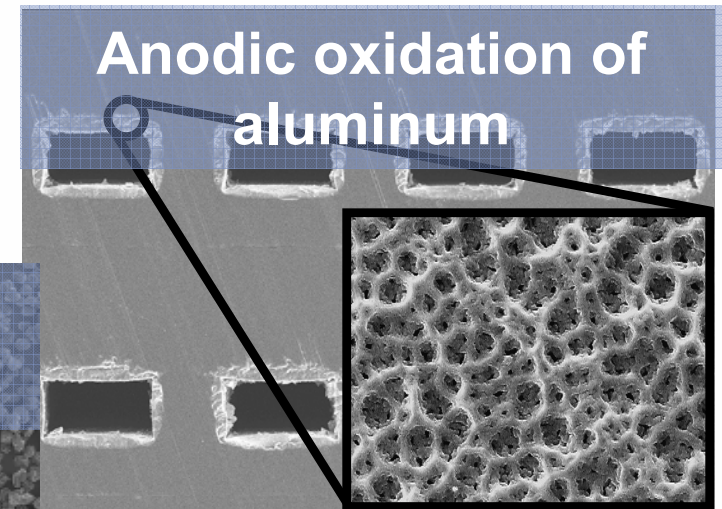
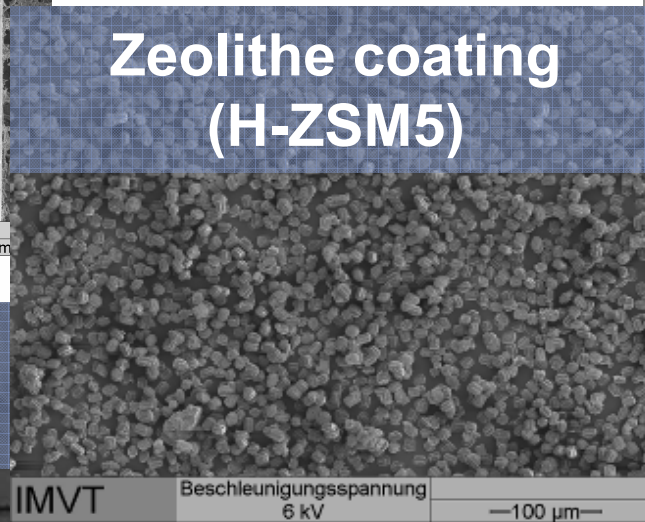
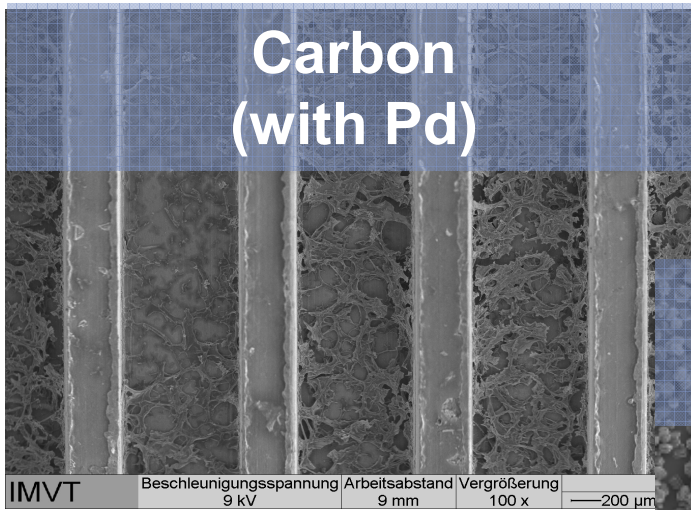
Methods of catalyst incorporation

- Packed structure with catalyst mixture (Cu/Zn/Al + H-ZSM5)

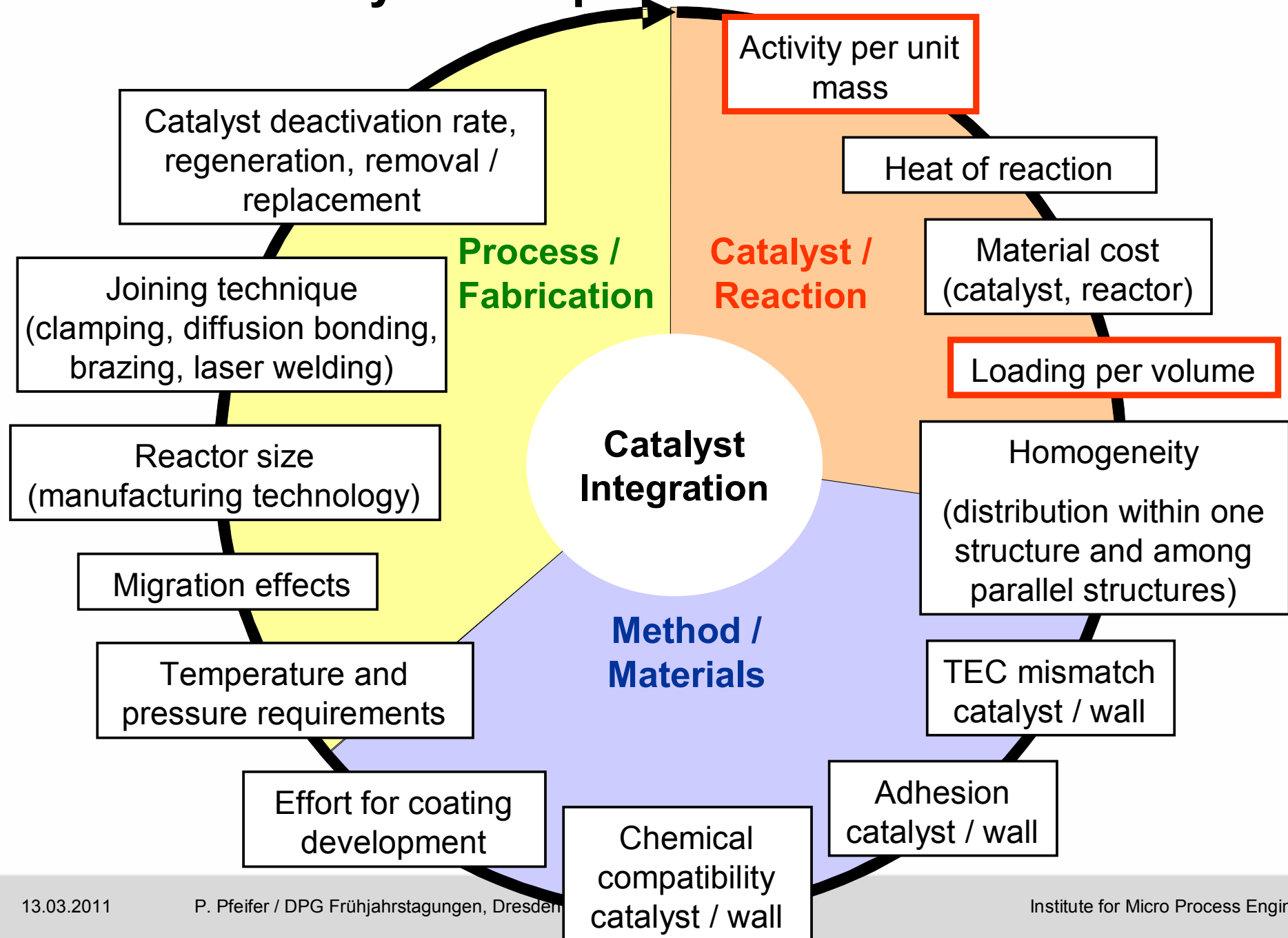


Methods of catalyst incorporation

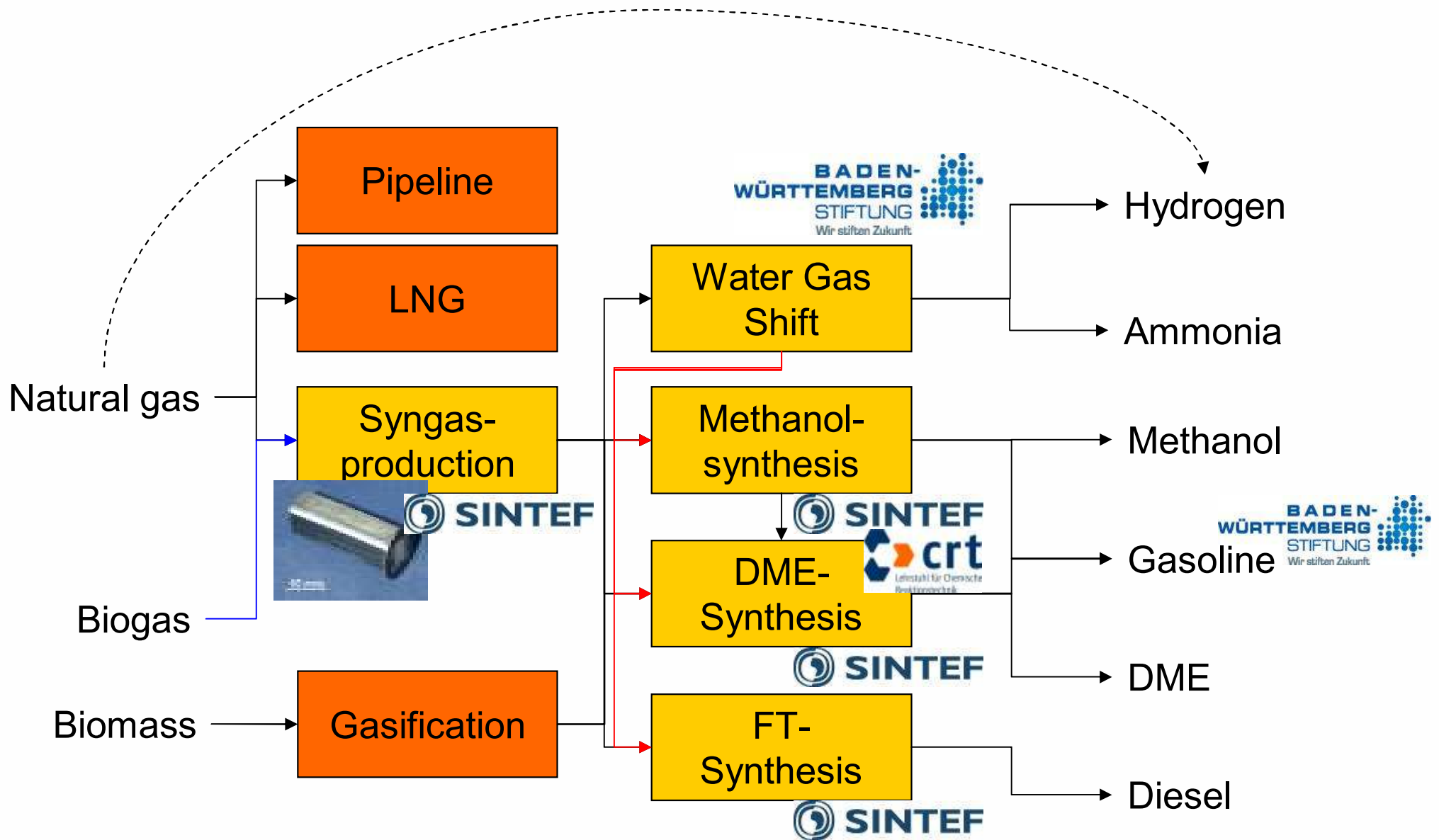
■ Coatings



Methods of catalyst incorporation - the decision?



Fuel routes and current projects

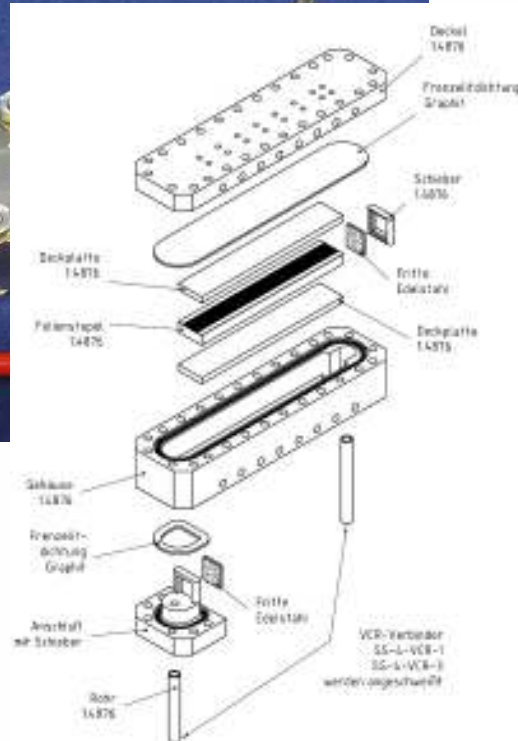
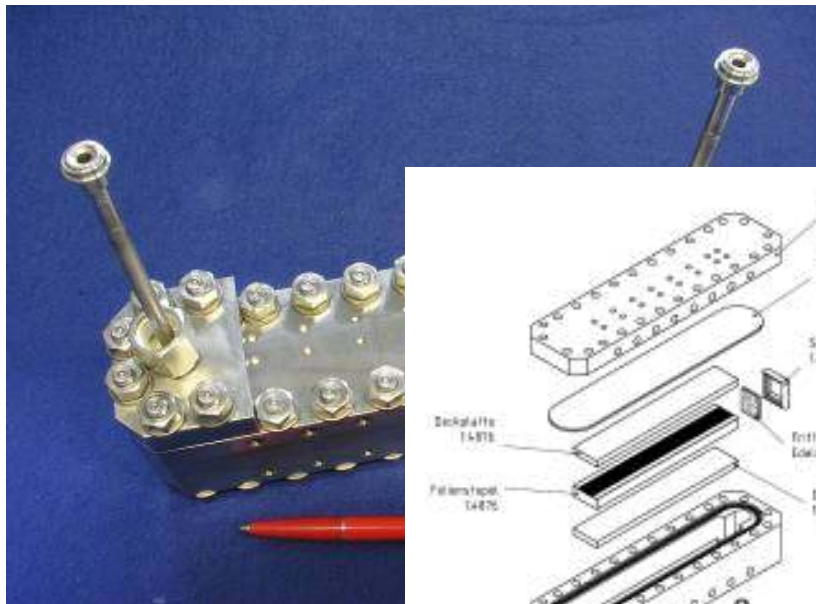


Reactor design for lab-scale testing

- Two different concepts

*Variable structure (coating+packing)
Electrically heated*

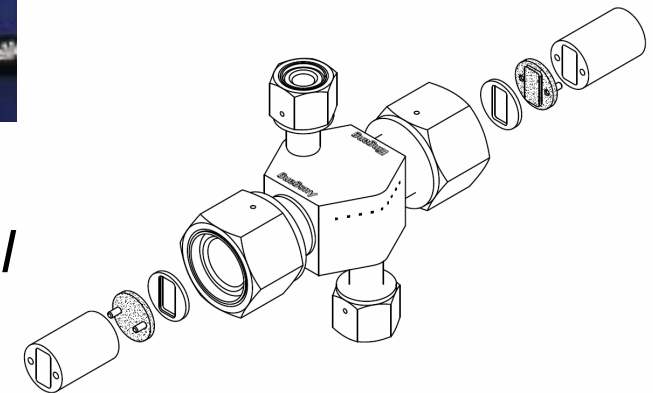
*Catalyst packing
Fluidic heating/cooling*



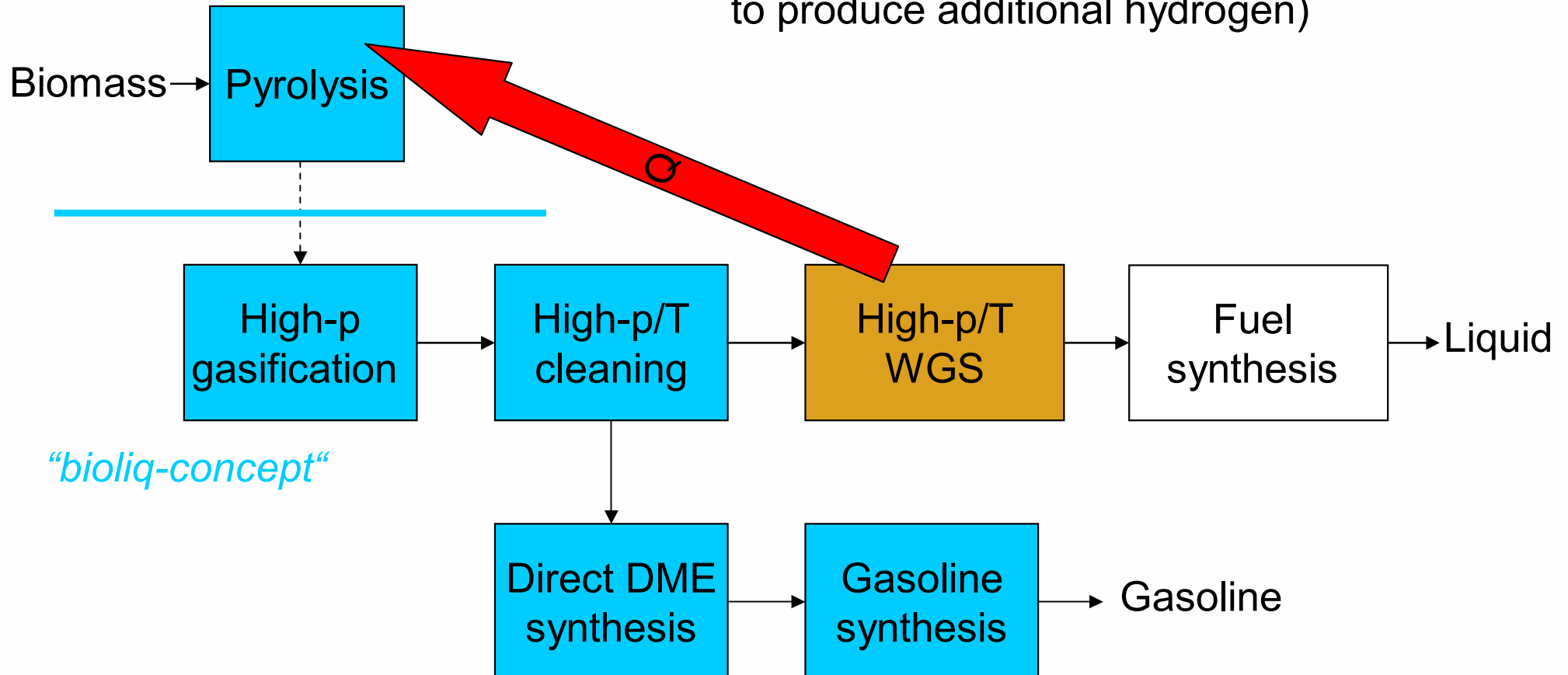
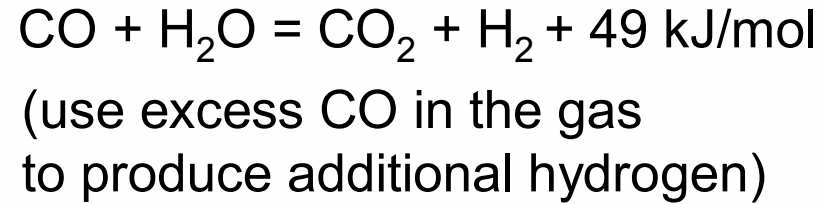
*Enabling
T-gradients*



*Strictly
isothermal*

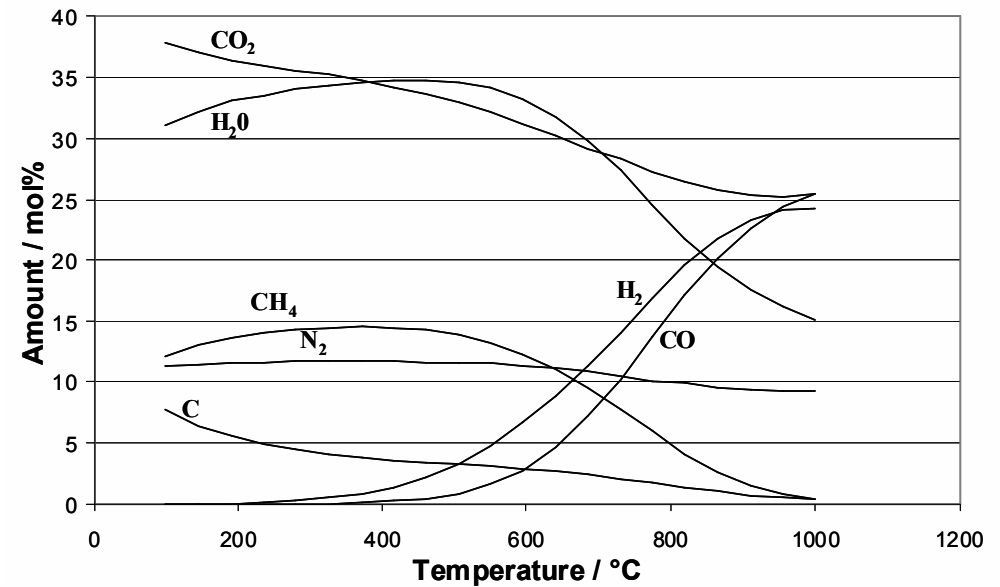
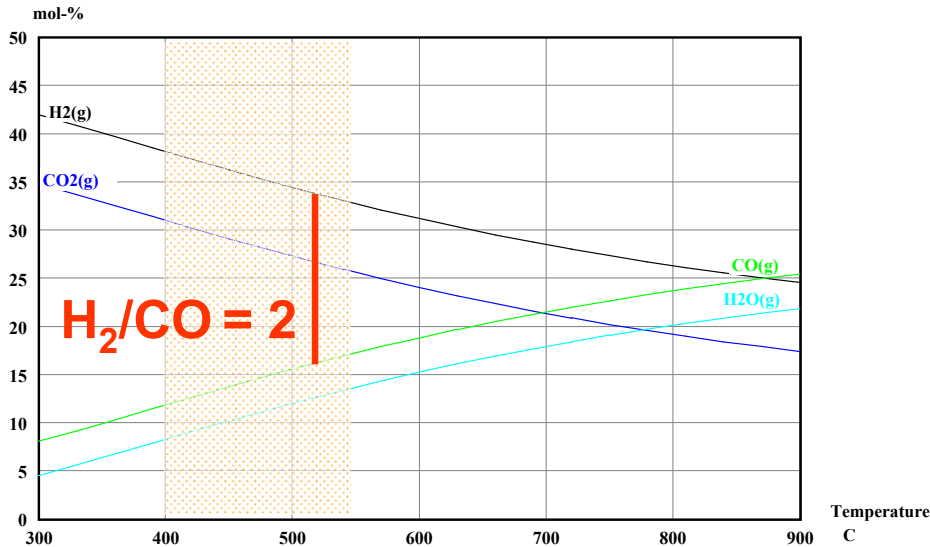


High-p high-T water gas shift



High-p high-T water gas shift

*Temperature region and importance of byproduct formation
(thermodynamics)*

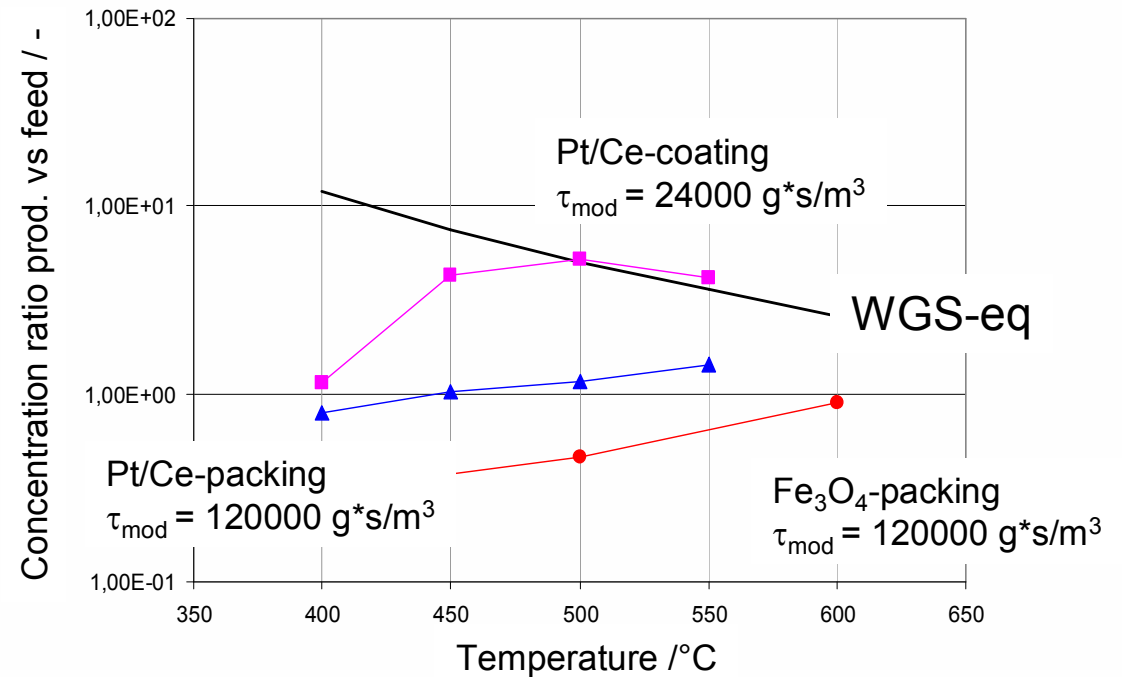
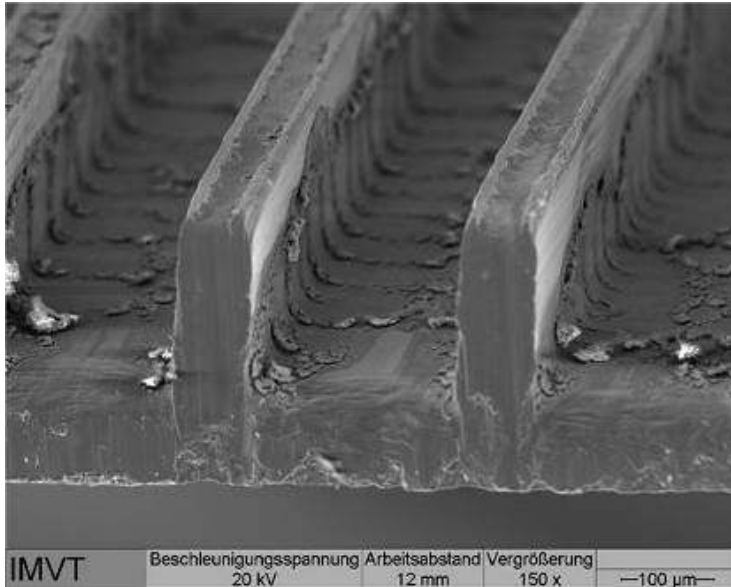


Feed: 32 % CO
18 % H₂
11 % CO
11 % N₂
28 % H₂O

Press.: 50 bar

High-p high-T water gas shift

- highly active wall coatings – 5% Pt/CeO₂ : up to 80 g_{CO}/gh



Pt/Ce/Al:

Pt/Ce:

	CH ₄ / Vol. %	ΣC ₂ + / Vol. %
1 bar	-	-
45 bar	2,82	0,91
1 bar	-	-
45 bar	2,39	0,63

High-p high-T water gas shift



REGA Gasifier



Filter

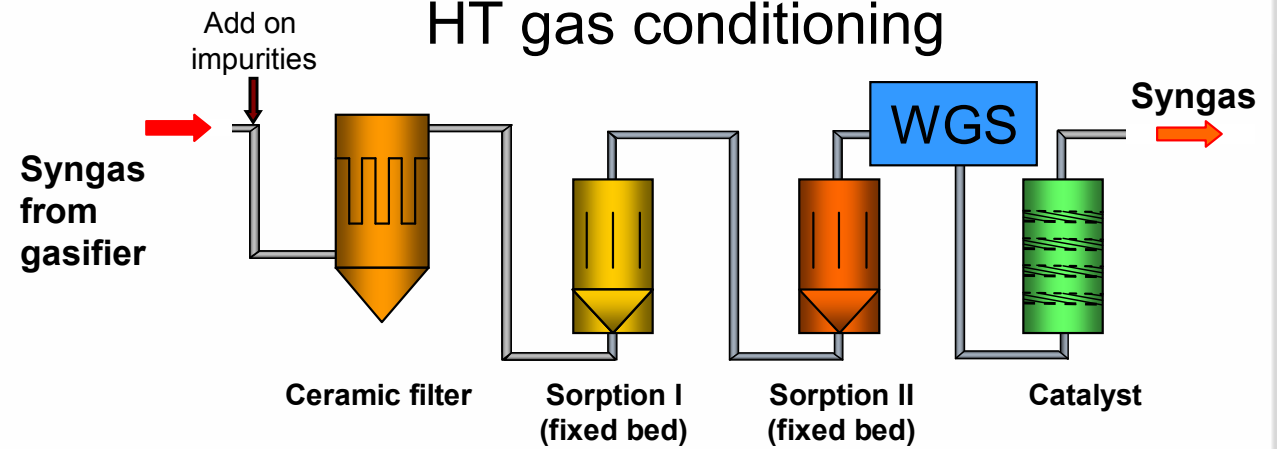


Sorption I

Sorption II

Catalyst

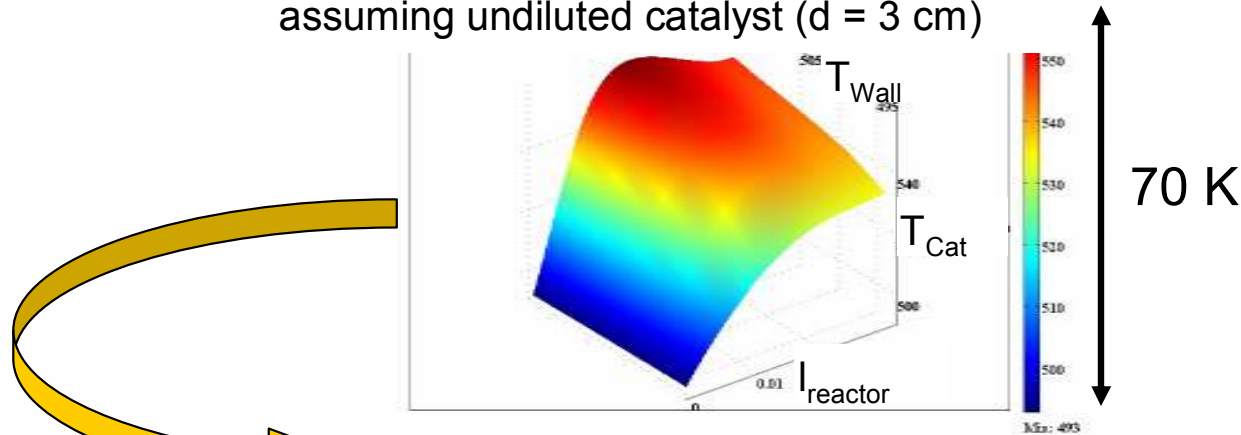
HT gas conditioning



WGS

Fischer-Tropsch synthesis

Simulated temperature distribution in a fixed bed reactor
assuming undiluted catalyst (d = 3 cm)



Reactor	Diluted fixed bed				Micro packed bed					
	A	A	A	B	A	A	B	B	B	B
Catalyst	A	A	A	B	A	A	B	B	B	B
Temperature [°C]	210	210	210	210	215	215	210	215	225	240
Pressure [bar]	20	20	20	20	20	20	20	20	20	20
GHSV [ml g ⁻¹ h ⁻¹]	11000	10600	5600	11700	13900	8750	12300	14400	14400	20548
Contact time [s]	0,33	0,34	0,64	0,31	0,25	0,41	0,29	0,25	0,25	0,18
CO-conv [%]	47	47	74	47	47	72	47	51	72	83
selC5+ [%]	84	84	85	85	83	86	84	83	84	82
selCH4 [%]	9	8	7	8	9	8	9	9	9	12
HCrates [g g ⁻¹ h ⁻¹]	1,0	1,0	0,8	1,1	1,3	1,3	1,1	1,5	2,1	3,4

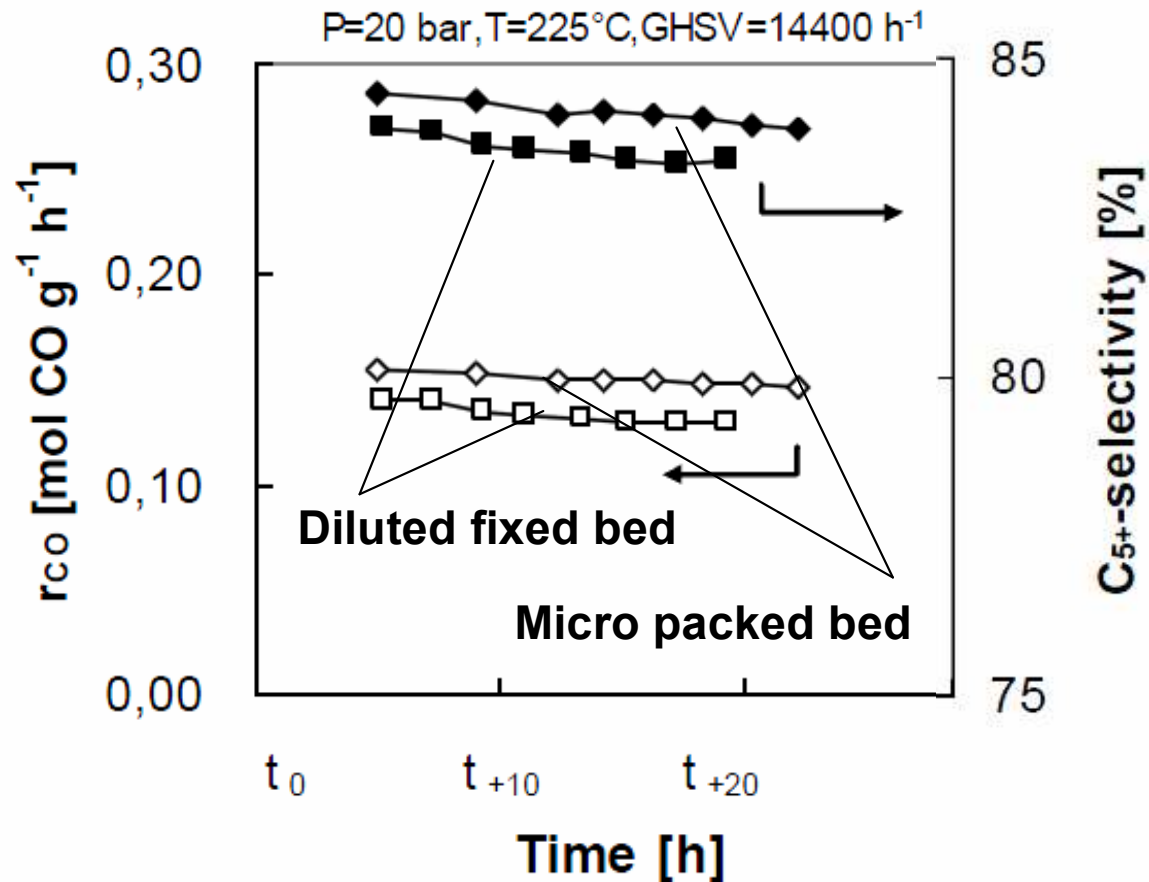
A: 20Co0.5Re on Al₂O₃

B: 20Co0.5Re5Ni on Al₂O₃

up to 50 % increase in space time yield possible (catalyst mass basis)
or at least reactor size reduction by 90 %

Fischer-Tropsch synthesis

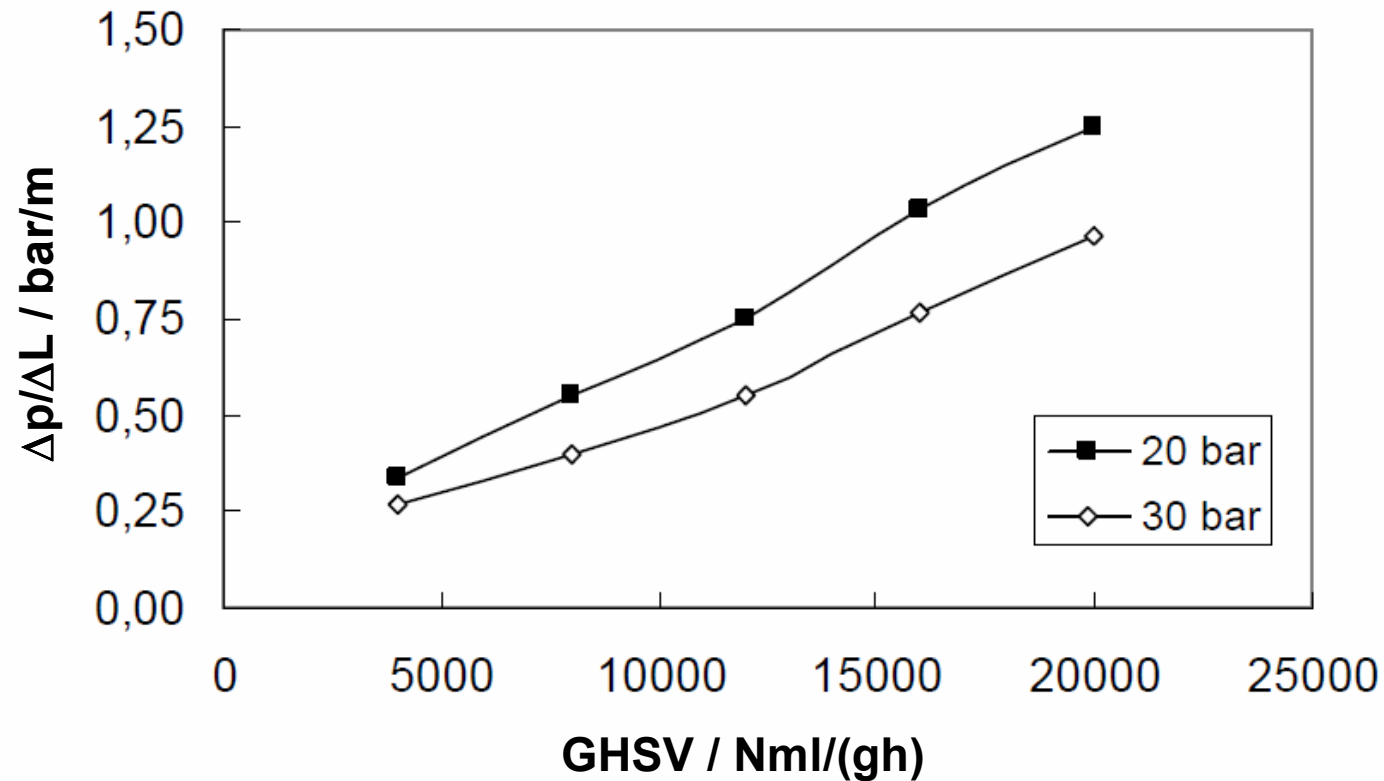
- Deactivation performance compared to conventional technology



=> No deactivation due to hot spots or wall effects !

Fischer-Tropsch synthesis

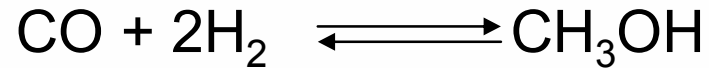
- Pressure drop at small particle size?



=> Negligible even at high bed length!

Myrstad et al., Catalysis Today 147S (2009) 301–S304

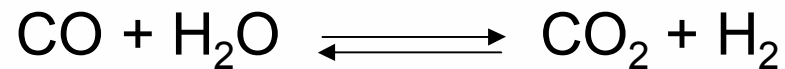
New catalysts for direct DME synthesis



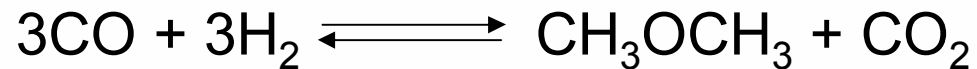
$$\Delta H_{\text{R}}^{298} = -90,4 \text{ kJ/mol}$$



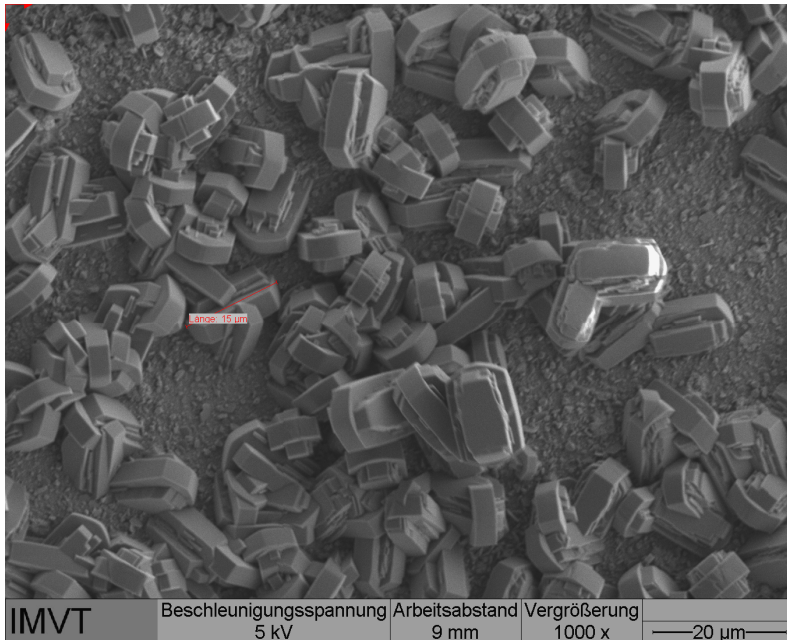
$$\Delta H_{\text{R}}^{298} = -23,0 \text{ kJ/mol}$$



$$\Delta H_{\text{R}}^{298} = -41 \text{ kJ/mol}$$



$$\Delta H_{\text{R}}^{298} = -244,8 \text{ kJ/mol}$$



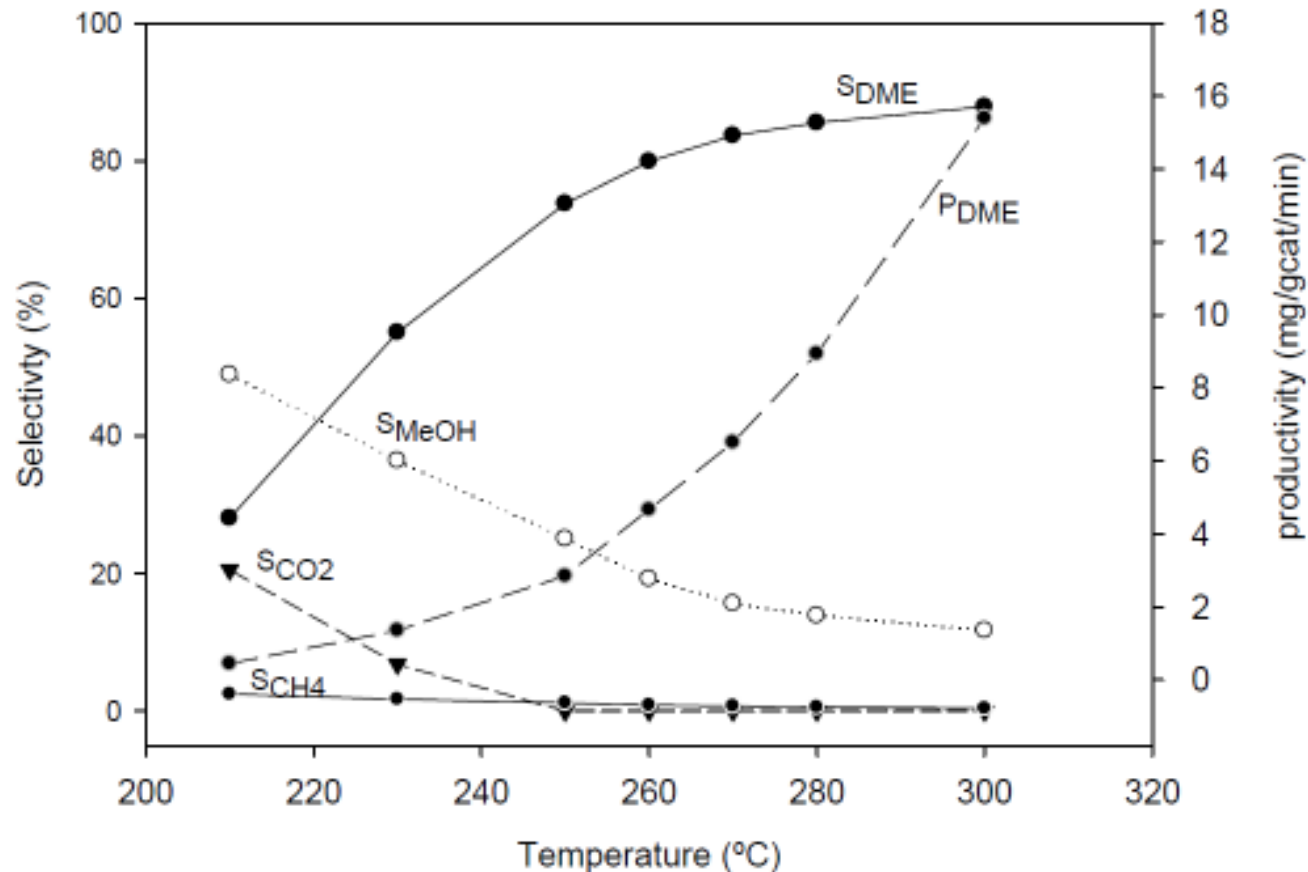
Coating with H-ZSM5 (dehydration)



New: Core-shell and double layer catalysts

DME direct synthesis

■ Results from Cu/Zn/Al + γ -Al₂O₃



Feed: 42 % H₂
 42 % CO
 5 % CO₂
 Rest N₂

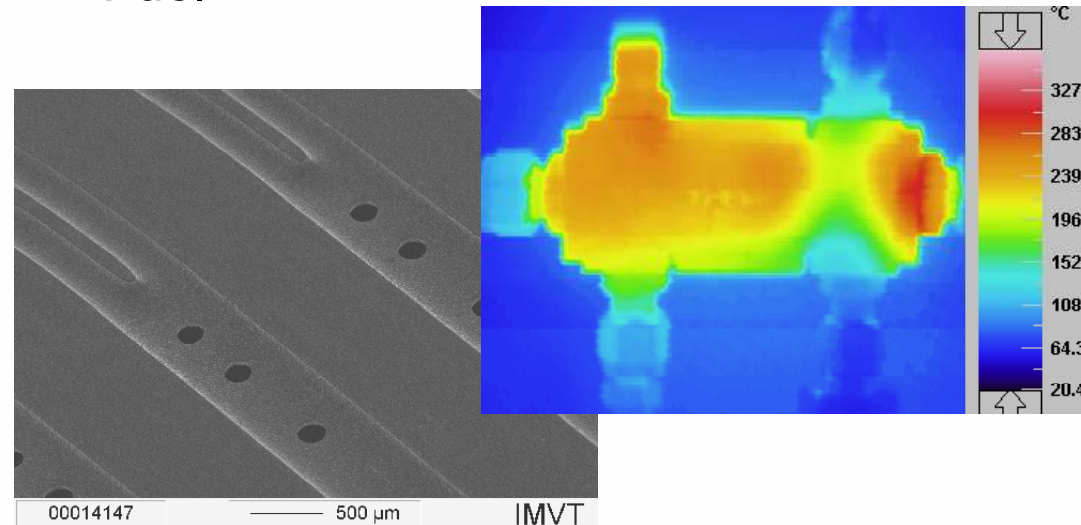
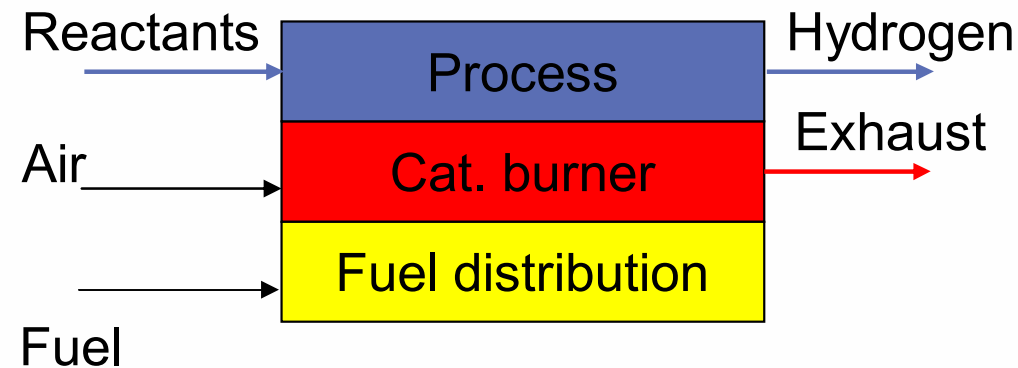
50 bar
 H₂:CO = 1
 SV = 15000 Nml/g_{cat}h

Hayer et al., Chem. Eng. J. (2010 online)

Hydrogen Production Processes

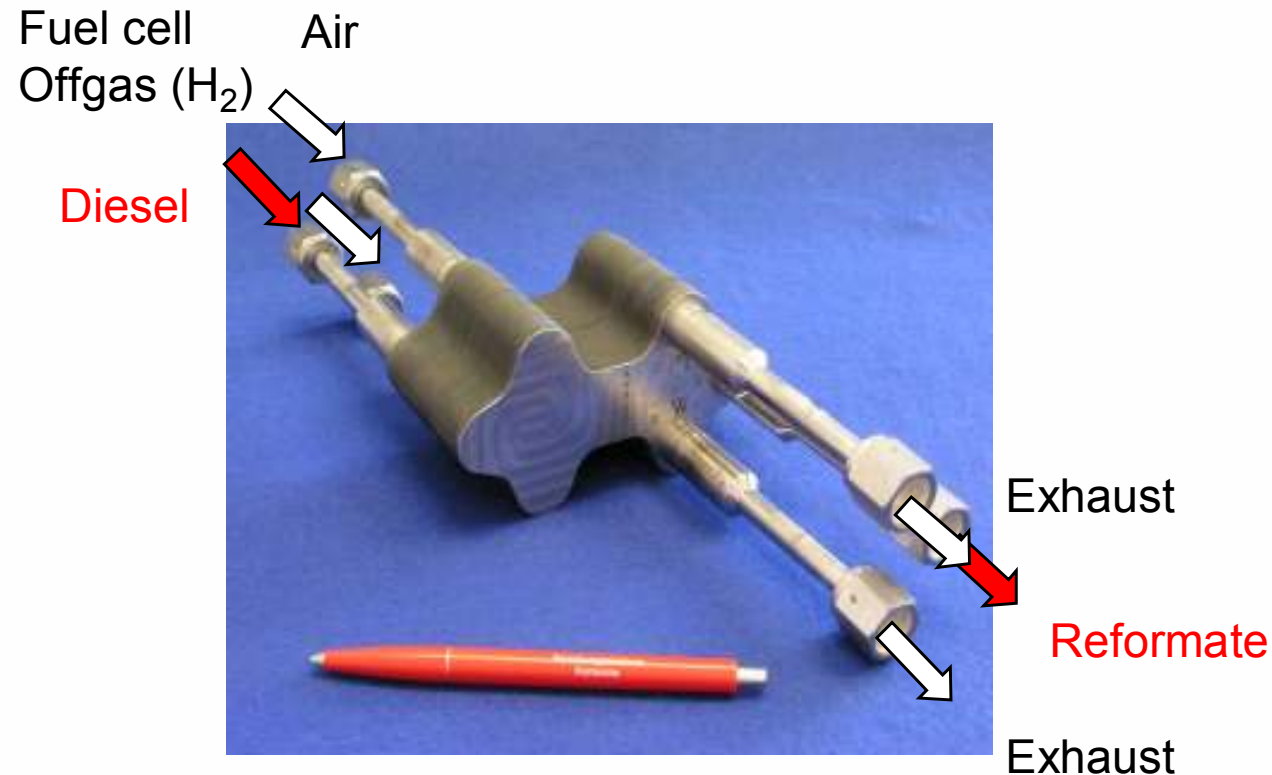
- Effectively coupling endo- und exothermic processes for increasing efficiency

Microreactor



Hydrogen Production Processes

- Example for a reactor with integrated combustion



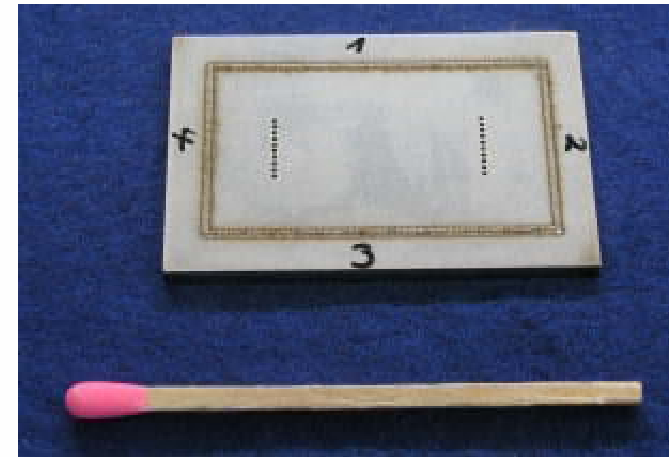
- Future step: Microreactors with integrated membrane for in-situ hydrogen separation of H_2 => synergies through
 - 1) Increase eq-conversion / increase of kinetics
 - 2) Stabilization of the membrane

Membrane integration

- Foil concept < 400°C



Foil obtained from CETH, Paris



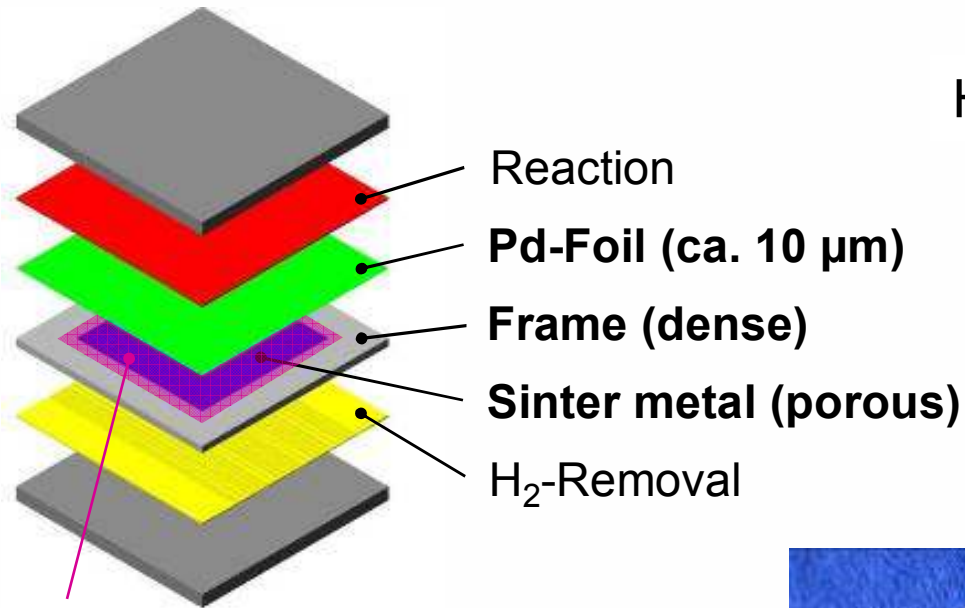
Laser welded unit
(Pd foil size: 40 x 27 mm²)



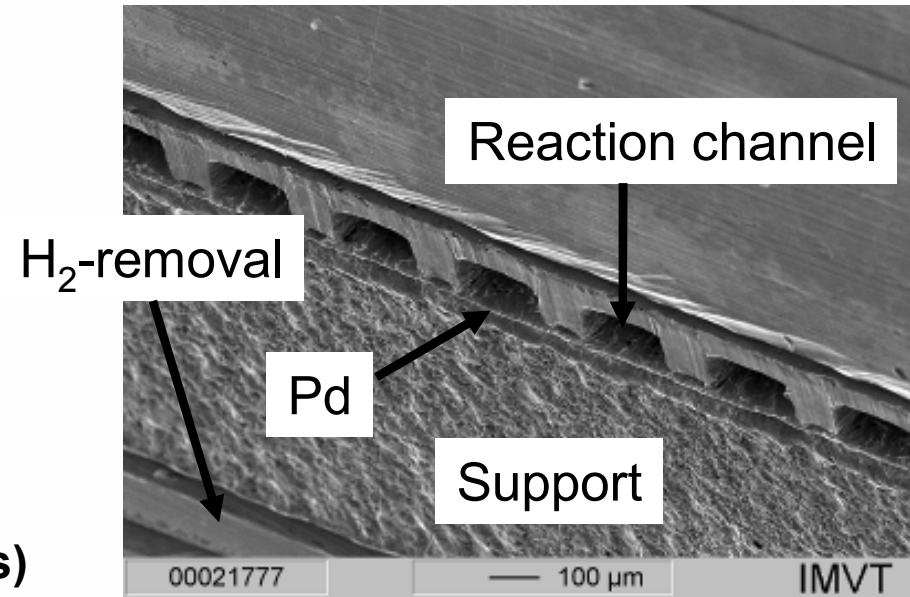
Test arrangement (elec. heated)

Membrane Integration

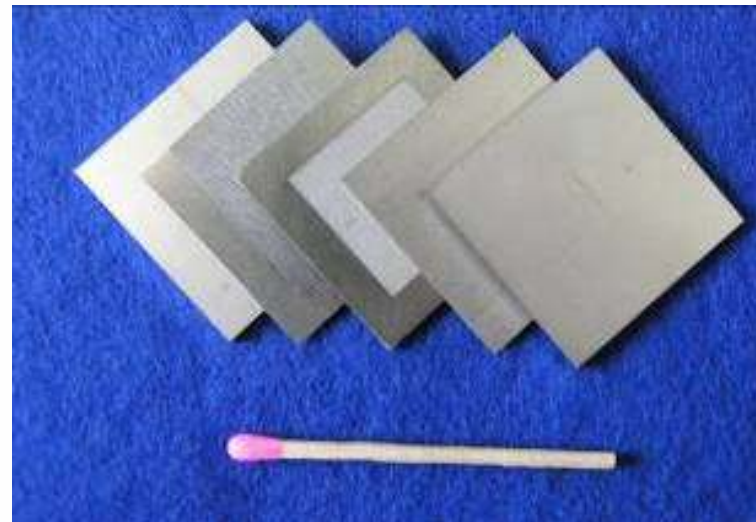
- Foil concept > 400°C



Porous inorganic barrier layer

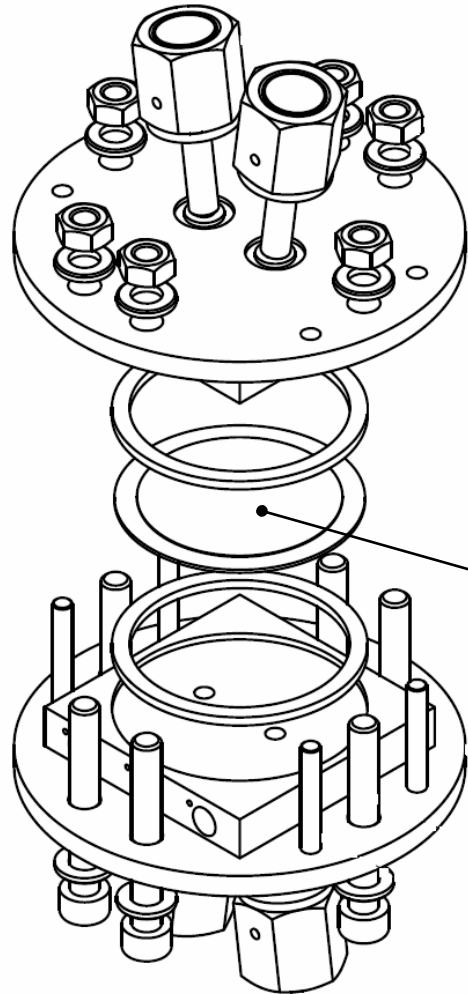


Diffusion bonded foils



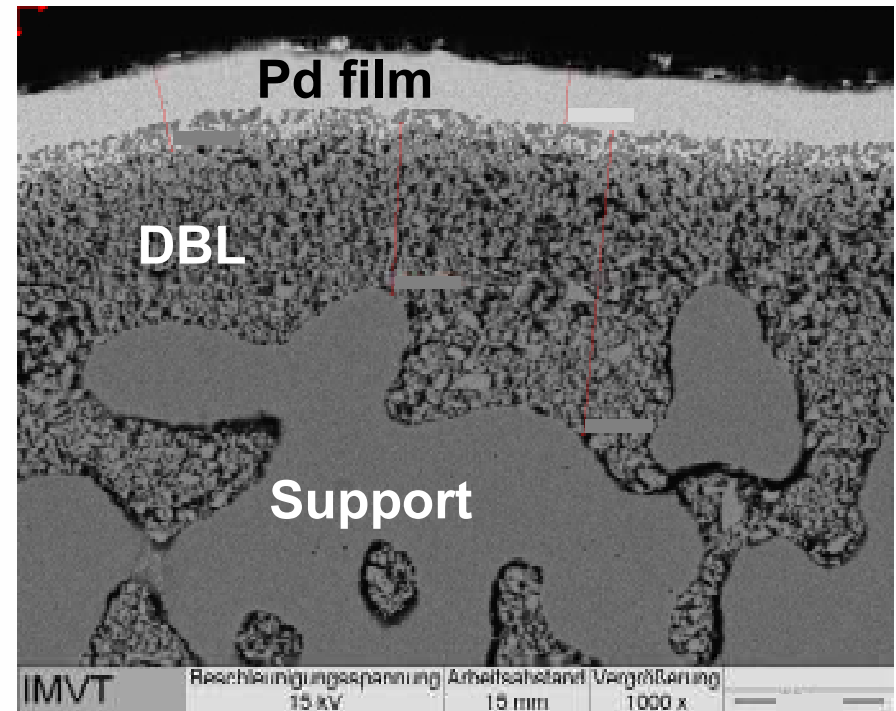
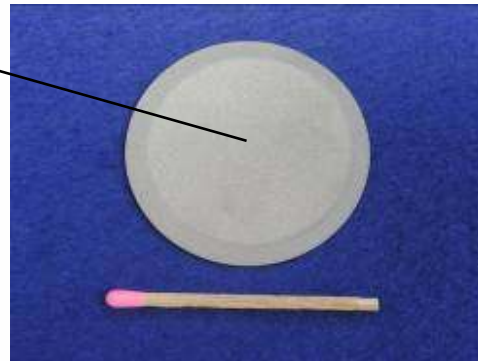
Membrane Integration

- Coating concept > 400°C



Pd thickness
5-15 μm

Pd penetrates
few microns
into DBL



Example: Pd by electroless plating

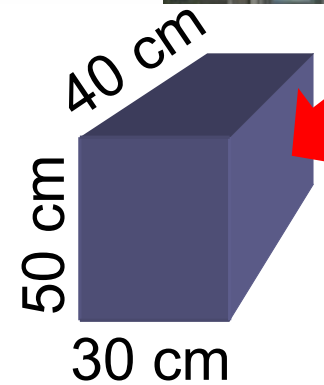
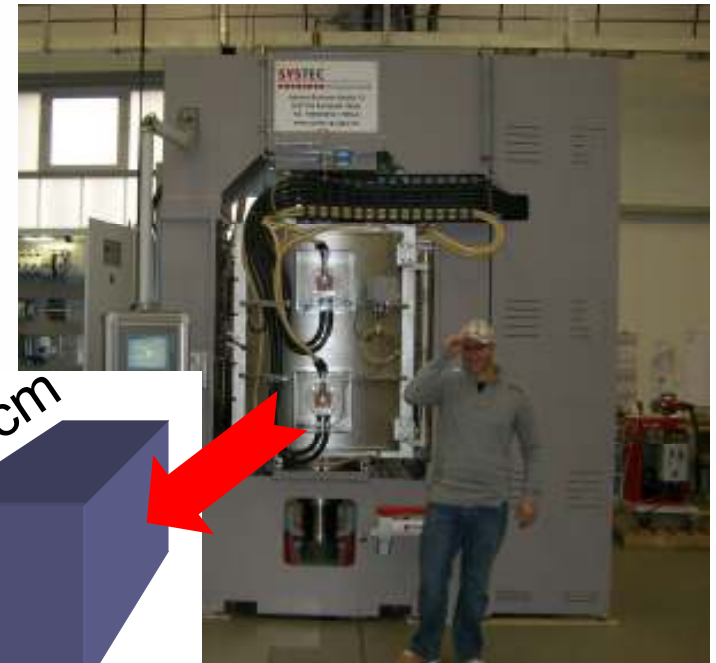
Test arrangement (electrically heated)

Scale-up / feasibility

Scale-Up

Scale today

Scale in 2011



2 g catalyst / lab

200 g catalyst / tech

~ 7-30 kg catalyst
for pilot scale FT-synthesis

Conclusions

- Advantages like temperature profiles for fuel synthesis
- Reactor designs, catalysts and possible applications
- New approaches with highly active catalysts
- Compact systems feasible
- Scale-up feasibilities – current state is promising

Pearl GTL project
www.arabianoilandgas.com



Thank you for your attention



and thanks to my team....

